



EU-Russia Regulatory Dialogue: Construction Sector Subgroup

Seminar

“Worked examples on Bridge Design with Eurocodes”

St-Petersburg, 17-18 April 2013

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TC250 Structural Eurocodes



Geotechnical aspects of bridge design (EN 1997)

Jean-Pierre Magnan
Dr.Sc., Prof., IGPEF
IFSTTAR & École nationale des ponts et chaussées
Marne-la-Vallée, France

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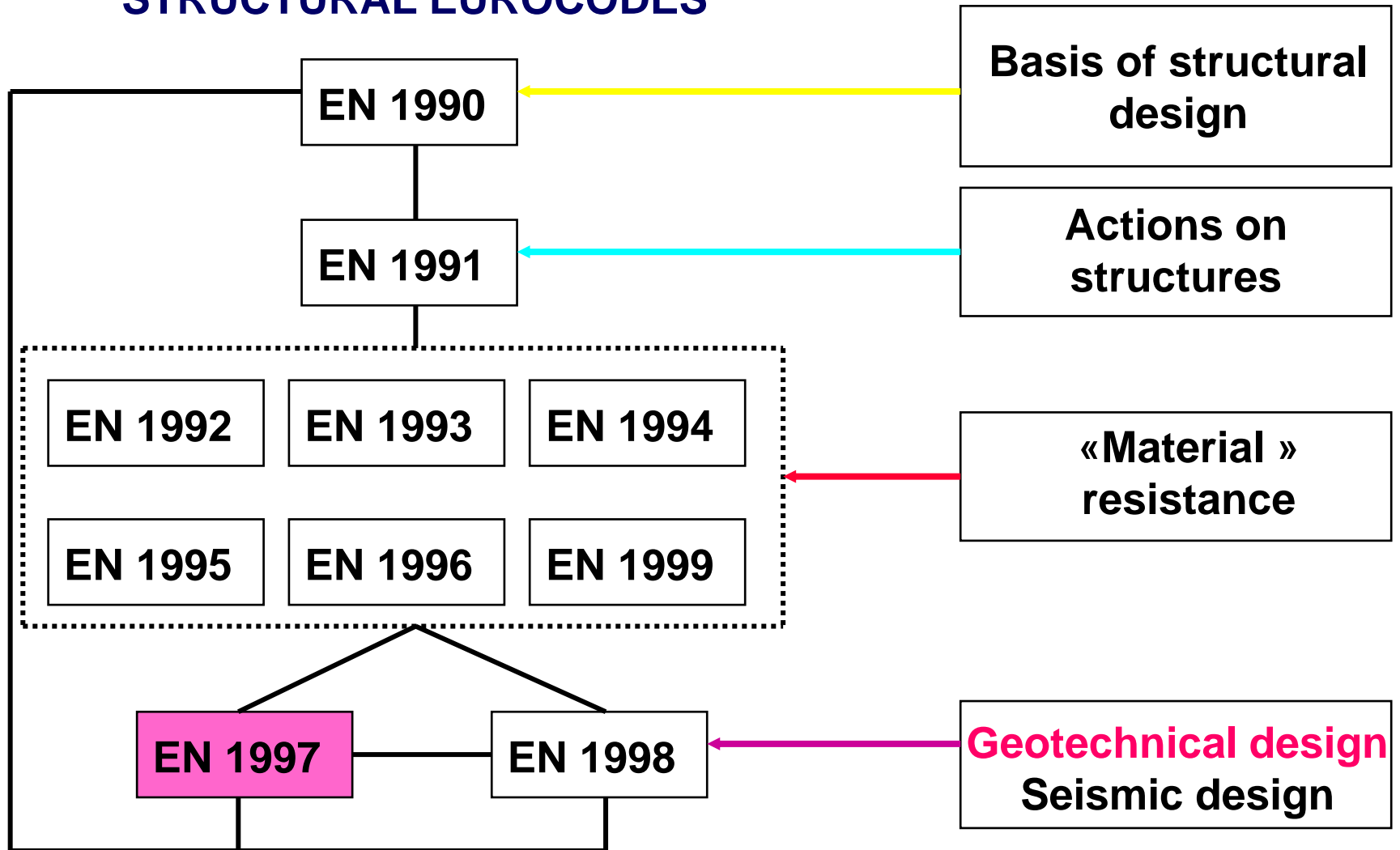
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STRUCTURAL EUROCODES





GEOTECHNICAL DESIGN / ANALYSIS

=

Checking all aspects of the interaction of a given structure and ground

Geotechnical analysis is responsible for

- **assessing the ground nature and properties, including water,**
- **defining the ground resistance to any load (vertical, inclined, static, dynamic, seismic),**
- **estimating the ground deformation produced by the structure or any external action,**
- **defining the interaction forces at the ground-structure interface,**
- **checking the site stability and durability.**

The aims of geotechnical analysis are the same in all countries.



NATIONAL EXPERIENCE AND EUROCODE 7

After a long (about 20 years) initial period trying to elaborate unified procedures, it was decided to produce an « umbrella » code giving rules but leaving details to national experience and preferences.

An example: The code says **”You shall make a geotechnical model of the site interacting with the structure”**. But the way to achieve this is not imposed: you may use geology, geophysics, hydrogeology, in situ testing, core sampling and laboratory testing... depending on the way structures are calculated at the end. For resistances, some countries like pressuremeter or cone penetrometer, others like « c and ϕ ».

EUROCODE 7 AND "DESIGN"

Eurocodes do not prescribe the type of structures nor their foundations. This bridge might be founded on piles, a piled raft, shallow foundations.

Eurocodes define rules that have to be applied to prove the quality of the designed structure: loads and load combinations, criteria to be met by actions and resistances, provisions for safety assurance.

Eurocode 7 defines the rules for all actions and resistances linked to the ground (in combination with EC8 Part 5 for seismic situations).

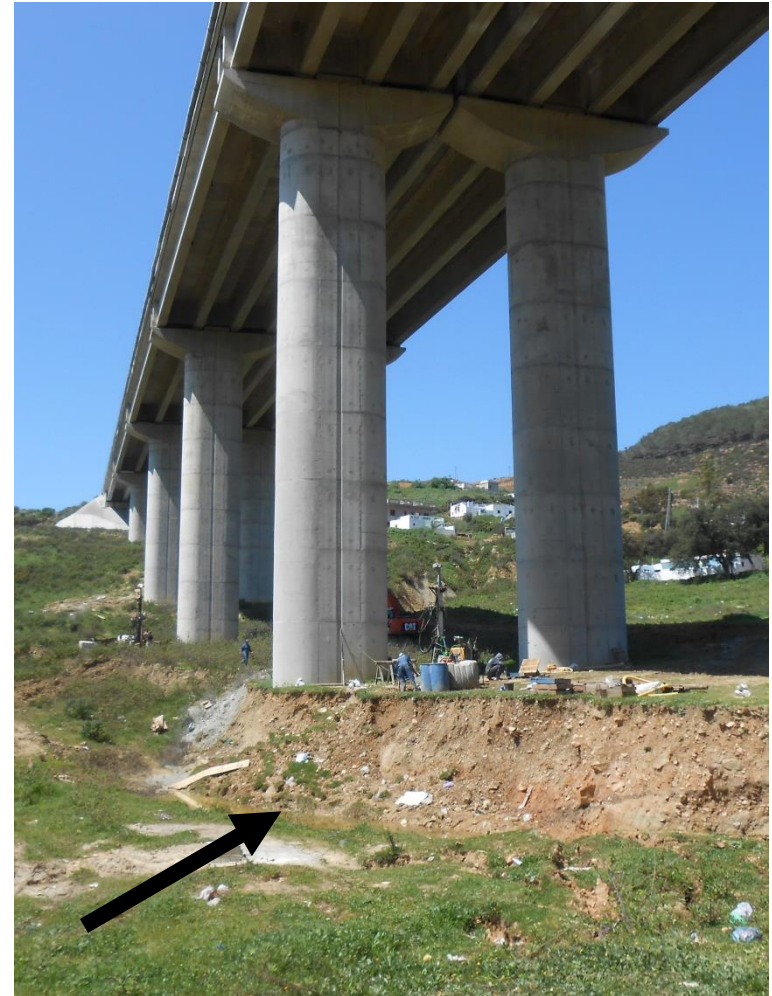
For bridges, the loads are those transmitted by the structure to ground.



EUROCODE 7 AND "DESIGN"

The reason which incited me to fly to Casablanca then drive to Tangiers in Morocco last Saturday was the development of a landslide next to the bridge foundation. A decision had to be taken: close or do not close the highway?

Even if Eurocodes tell which conditions have to be met, they don't indicate how groups of piles function next to a landslide, which could eventually cross the bridge. The decision rely on the engineers understanding of nature.





Eurocode 7 – Geotechnical design (applied to buildings and bridges)

EN 1997-1 (2004) : Part 1 - General rules

EN 1997-2 (2007) : Part 2 - Ground investigation and testing

Contents of Part 1 (EN 1997-1:2004)



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- Section 1 General
- Section 2 Basis of geotechnical design
- Section 3 Geotechnical data
- Section 4 Supervision of construction, monitoring and maintenance
- Section 5 Fill, dewatering, ground improvement and reinforcement
- Section 6 **Spread foundations**
- Section 7 **Pile foundations**
- Section 8 **Anchorage**
- Section 9 **Retaining structures**
- Section 10 Hydraulic failure
- Section 11 Site stability
- Section 12 Embankments
- Informative annexes with some calculation methods and recommended values of γ 's

EUROPEAN STANDARD
NORME EUROPÉENNE
EUROPÄISCHE NORM

EN 1997-1

November 2004

ICS 91.120.20

Supersedes ENV 1997-1:1994

English version

Eurocode 7: Geotechnical design – Part 1: General rules

Eurocode 7: Calcul géotechnique – Partie 1: Règles générales

Eurocode 7: Erdbau, Berechnung und Bemessung in der Geotechnik – Teil 1: Allgemeine Regeln

This European Standard was approved by CEN on 23 April 2004.

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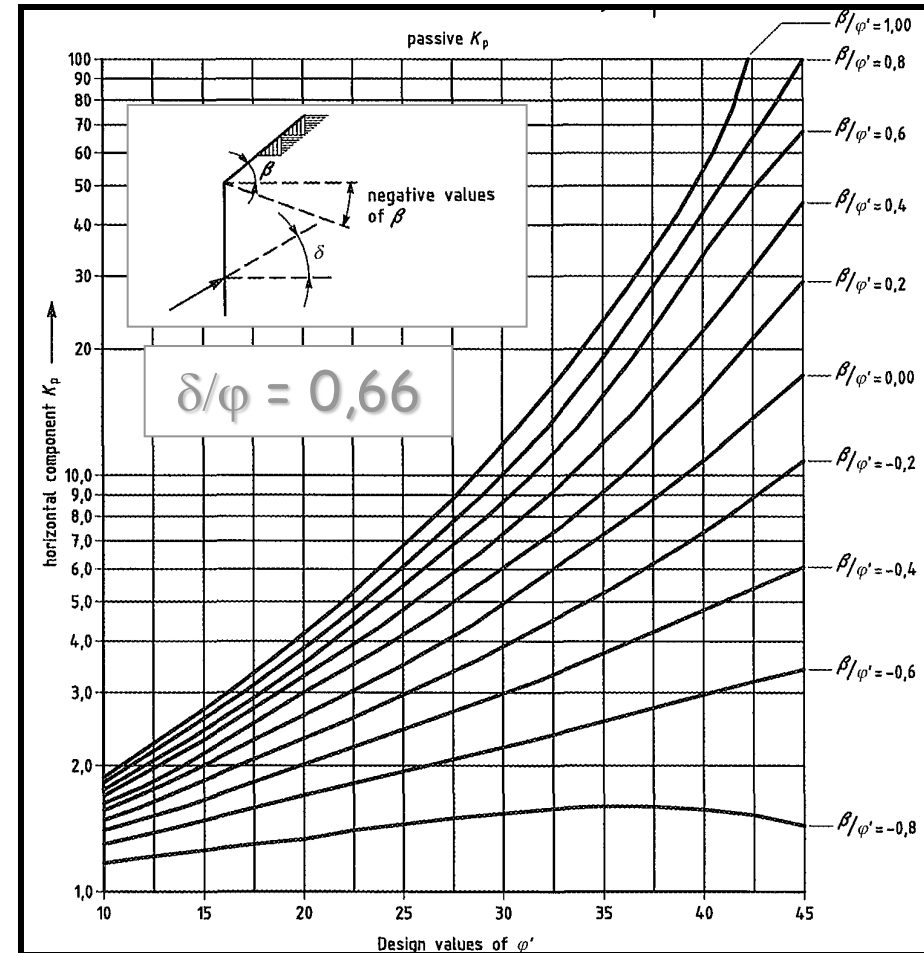
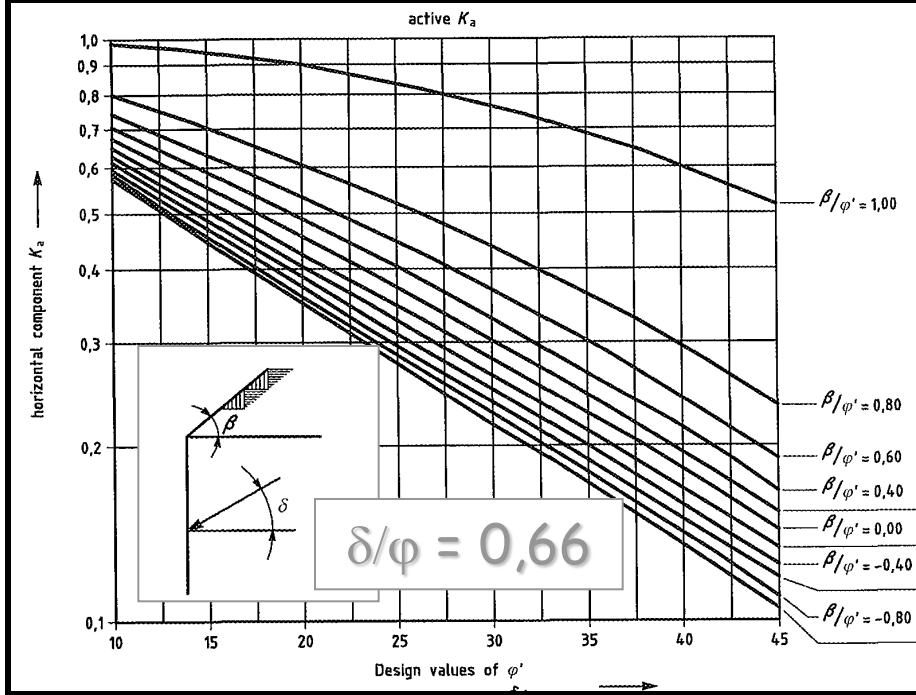
Ref. No. EN 1997-1:2004: E

Active /Passive earth pressures - annex C (Informative)



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Active/Passive earth pressures

$$\beta = -\varphi \text{ à } +\varphi$$

$$\delta = 0 ; 2/3\varphi \text{ and } \varphi$$

Ground resistance (footings)

“c-φ” model (Annex D)

$$R/A' = c' \times N_c \times b_c \times s_c \times i_c$$

$$+ q' \times N_q \times b_q \times s_q \times i_q$$

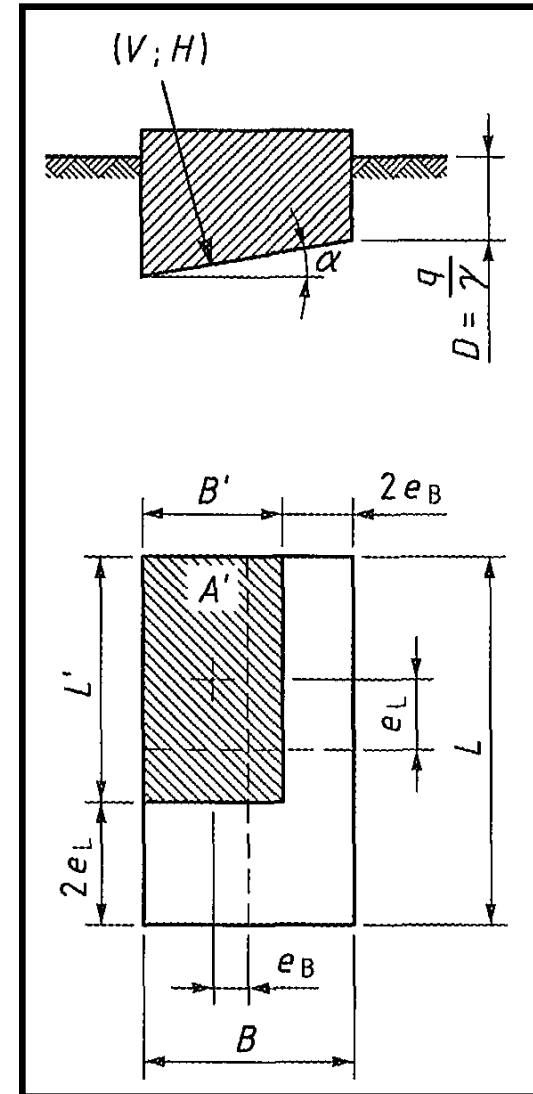
$$+ 0,5 \times \gamma \times B' \times N_\gamma \times b_\gamma \times s_\gamma \times i_\gamma$$

Pressuremeter model (Annex E)

$$R/A' = \sigma_{v0} + k \times p_{le}^*$$

Settlement of footings (Annex F)

$$\text{Adjusted elasticity: } s = p \times b \times f / E_m$$



Contents of Part 2 (EN 1997-2:2007)



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- Section 1 General
- Section 2 Planning and reporting of ground investigations
- Section 3 Drilling, sampling and groundwater measurements
- Section 4 **Field tests** in soils and rocks
- Section 5 **Laboratory tests** on soils and rocks
- Section 6 Ground investigation report
- Informative annexes
- (including calculation methods for piles)**

EUROPEAN STANDARD **EN 1997-2**
NORME EUROPÉENNE
EUROPÄISCHE NORM

March 2007

ICS 91.050.01; 91.120.20 Supersedes ENV 1997-2:1995, ENV 1997-3:1999

English Version

Eurocode 7 - Geotechnical design - Part 2: Ground investigation and testing

Eurocode 7 - Calcul géotechnique - Partie 2: Reconnaissance des terrains et essais Eurocode 7 - Entwurf, Berechnung und Bemessung in der Geotechnik - Teil 2: Erkundung und Untersuchung des Baugrunds

This European Standard was approved by CEN on 12 June 2006.

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Specific aspects of Eurocode 7-1



Characteristic values and design values

ULS and Design Approaches

SLS and deformations of structures



P The **characteristic value** of a geotechnical parameter shall be selected as a cautious estimate of the value affecting the occurrence of the limit state. They are therefore dependant of the structure to be designed.

If **statistical methods** are used, the characteristic value should be derived such that the calculated probability of a worse value governing the occurrence of the limit state under consideration is not greater than 5%.

Comment: Characteristic values of ground properties are considered to be the same as the values previously used for geotechnical calculations.



Design values are obtained from characteristic values by using partial factors:

Effects (E) of Actions (F) are

increased when unfavourable $E_d = E_k \gamma_E (\gamma_E > 1)$,
decreased when favourable $E_d = E_k \gamma_E (\gamma_E < 1)$.

Resistances R and soil strength X_{mat} are usually decreased:

$$R_d = R_k / \gamma_R$$
$$X_{mat,d} = X_{mat,k} / \gamma_M$$

Combinations of actions for the structure are accepted as there are defined by structural engineers (EN1900, EN1901).



- **EQU** : loss of equilibrium of the structure
- **STR** : internal failure or excessive deformation of the structure or structural elements
- **GEO** : failure or excessive deformation of the ground
- **UPL** : loss of equilibrium due to uplift by water pressure (buoyancy) or other vertical actions
- **HYD** : hydraulic heave, internal erosion and piping caused by hydraulic gradients

(Fatigue is not considered)



Limit states may be checked (avoided) by one or more of the following means:

- by calculation (section 2.4);
- by prescriptive measures (section 2.5);
- by testing models or load tests (section 2.6);
- by an observational method (section 2.7).

Checking stability by calculation



Design values of geotechnical parameters

Design value of a parameter : $X_d = X_k / \gamma_M$

Design values of effects of actions and resistances

Checking for STR/GEO ULS :

$$E_d \leq R_d$$

$$E_d = E \{ \gamma_F \cdot F_k ; X_k / \gamma_M \} \quad \text{and} \quad R_d = R \{ \gamma_F \cdot F_k ; X_k / \gamma_M \}$$

(= “at the source”)

or
$$E_d = \gamma_E \cdot E \{ F_k ; X_k \} \quad \text{and} \quad R_d = R \{ F_k ; X_k \} / \gamma_R$$



Verifications :

$$E_d \leq C_d$$

C_d = limiting design value of the relevant serviceability criterion (eg settlements, relative rotations, etc.)

E_d = design value of the effects of actions specified in the serviceability criterion, determined on the basis of the relevant combination

all γ_F and $\gamma_M = 1.0$



Bearing resistance:

$$V_d \leq R_d = R_k / \gamma_{R;v}$$

(R_k : analytical – Annex D, semi-empirical – Annex E or prescriptive - Annex G)

Sliding resistance :

$$H_d \leq R_d + R_{p;d} \quad (R_p = \text{lateral resistance})$$

[+ $R_d \leq 0,4 V_d$ for undrained analysis]

- drained conditions :

$$R_d = V'_d \tan \delta_d \quad \underline{\text{or}} \quad R_d = (V'_d \tan \delta_k) / \gamma_{R;h}$$

- undrained conditions

$$R_d = A'c_{u;d} \quad \underline{\text{or}} \quad R_d = (A'c_{u;k}) / \gamma_{R;h}$$



Overall stability (“slope stability”)

Large eccentricities : special precautions if :
 $e/B > 1/3$ (or $0,6 \phi$)

Structural failure due to foundation movement

Structural design of spread foundation:
see EN 1992



What are the values of all the “ γ ” for geotechnical design ?

1. The partial factors are meant to assure safety.
2. Safety cannot be invented and must be referred to experience.
3. Soil mechanics has always used one global factor applied to resistances, without increasing loads. Therefore, design forces (or pressures) at the interface of ground and structure are discontinuous since structural design usually increases them by 1.35 or more.
4. The continuity at ground-structure interface implies that 1.35 should be introduced in geotechnical design. Most of CEN members accepted that, but not all countries. Two types of analyses, named “design approaches”, were then defined: Approach 1 specifies two parallel sets of calculations. Approach 2 (and approach 3, which differs by the position of partial factors) specifies only one set of calculations.

STR/GEO persistent and transient design situations (spread foundations without geotechnical actions)



Design approach	Actions on/from the structure γ_F	Geotechnical resistance γ_R or γ_M (at the source)
1	1,35 and 1,5 New	$\gamma_{R;v} = 1,0$ $\gamma_{R;h} = 1,0$
	1,0 and 1,3 Traditional	$\gamma_M = 1,25$ (on c' and $\tan\phi'$) or $\gamma_M = 1,4$ (on c_u)
2	1,35 and 1,5 New	$\gamma_{R;v} = 1,4$ $\gamma_{R;h} = 1,1$
3	1,35 and 1,5 New	$\gamma_M = 1,25$ (on c' and $\tan\phi'$) or $\gamma_M = 1,4$ (on c_u)

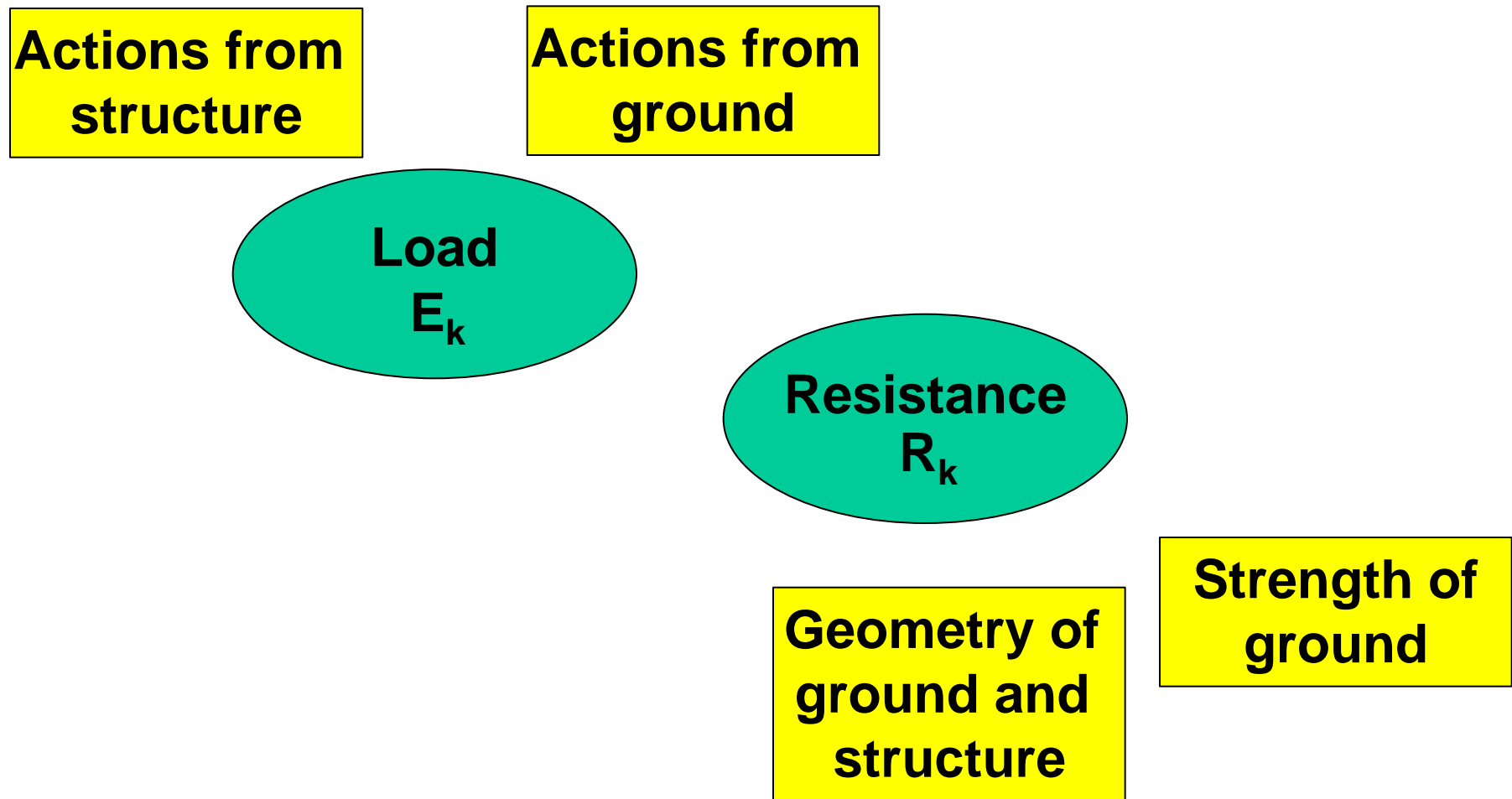
STR/GEO persistent and transient design situations (spread foundations without geotechnical actions)



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Experience (national) links safety to a minimum value of the ratio of resistances to loads.



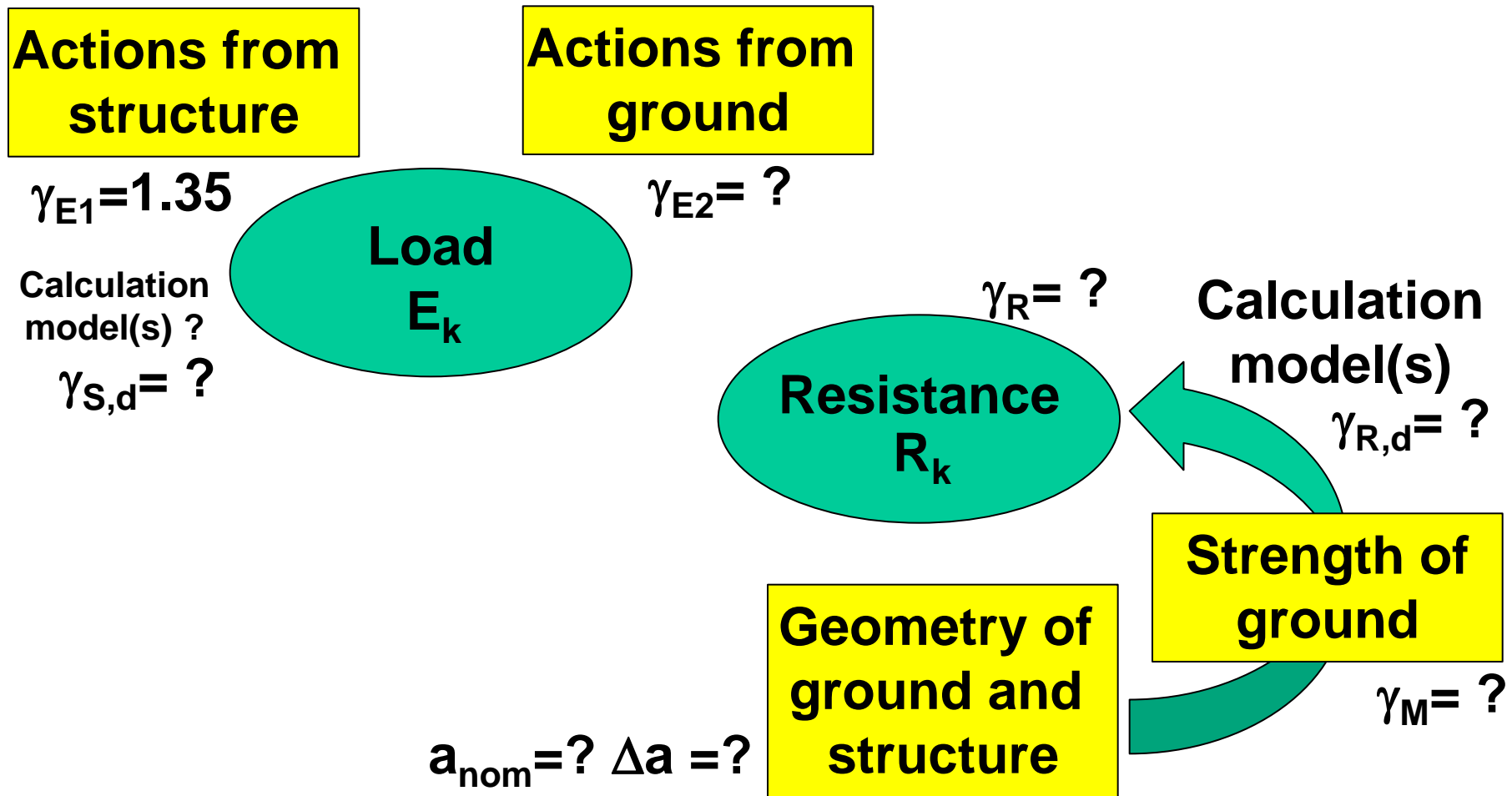
STR/GEO persistent and transient design situations (spread foundations without geotechnical actions)



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Question: how to divide existing global factors into partial ones to get an equivalent result?



STR/GEO persistent and transient design situations (spread foundations without geotechnical actions)



Design approach	Actions on/from the structure γ_F	Geotechnical resistance γ_R or γ_M (at the source)
1	1,35 and 1,5 New	$\gamma_{R;v} = 1,0$ $\gamma_{R;h} = 1,0$
	1,0 and 1,3 Traditional	$\gamma_M = 1,25$ (on c' and $\tan\phi'$) or $\gamma_M = 1,4$ (on c_u)
2	1,35 and 1,5 New	$\gamma_{R;v} = 1,4$ $\gamma_{R;h} = 1,1$
3	1,35 and 1,5 New	$\gamma_M = 1,25$ (on c' and $\tan\phi'$) or $\gamma_M = 1,4$ (on c_u)

Serviceability limit states (SLS)



Include both immediate and delayed settlements

Assess differential settlements and relative rotations

Check that limit values for the structure are not reached

frequent questions to structural engineers : what are they?...

Bridge design



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Bridge design



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Bridge design

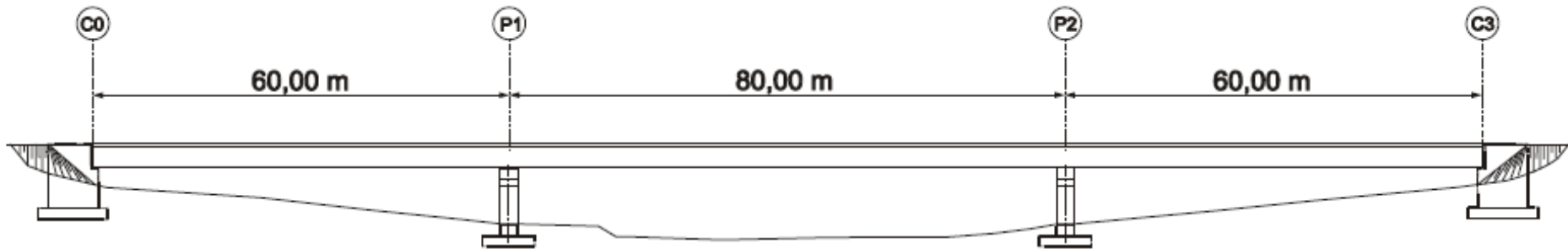


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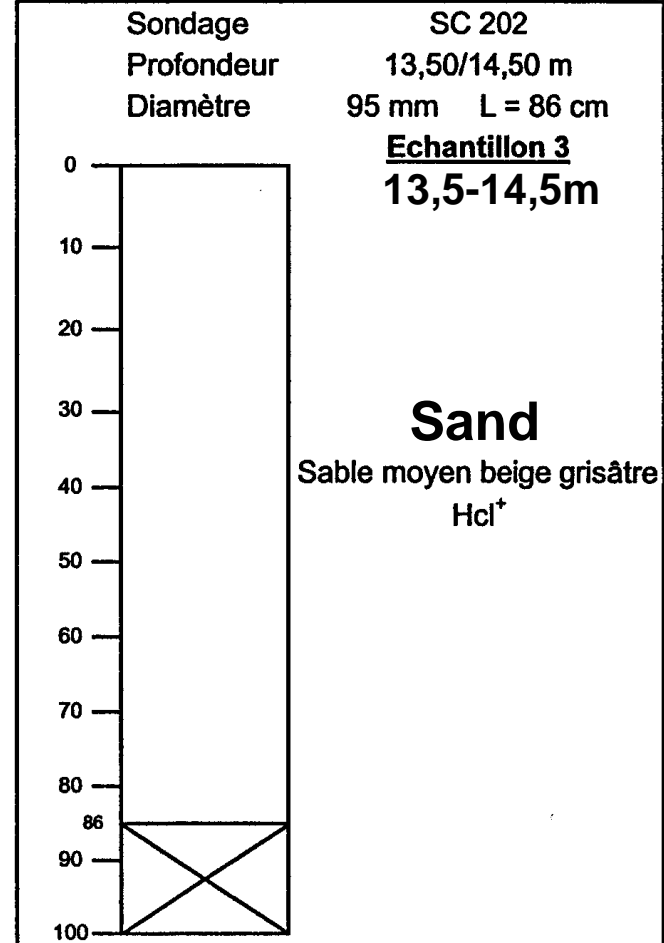
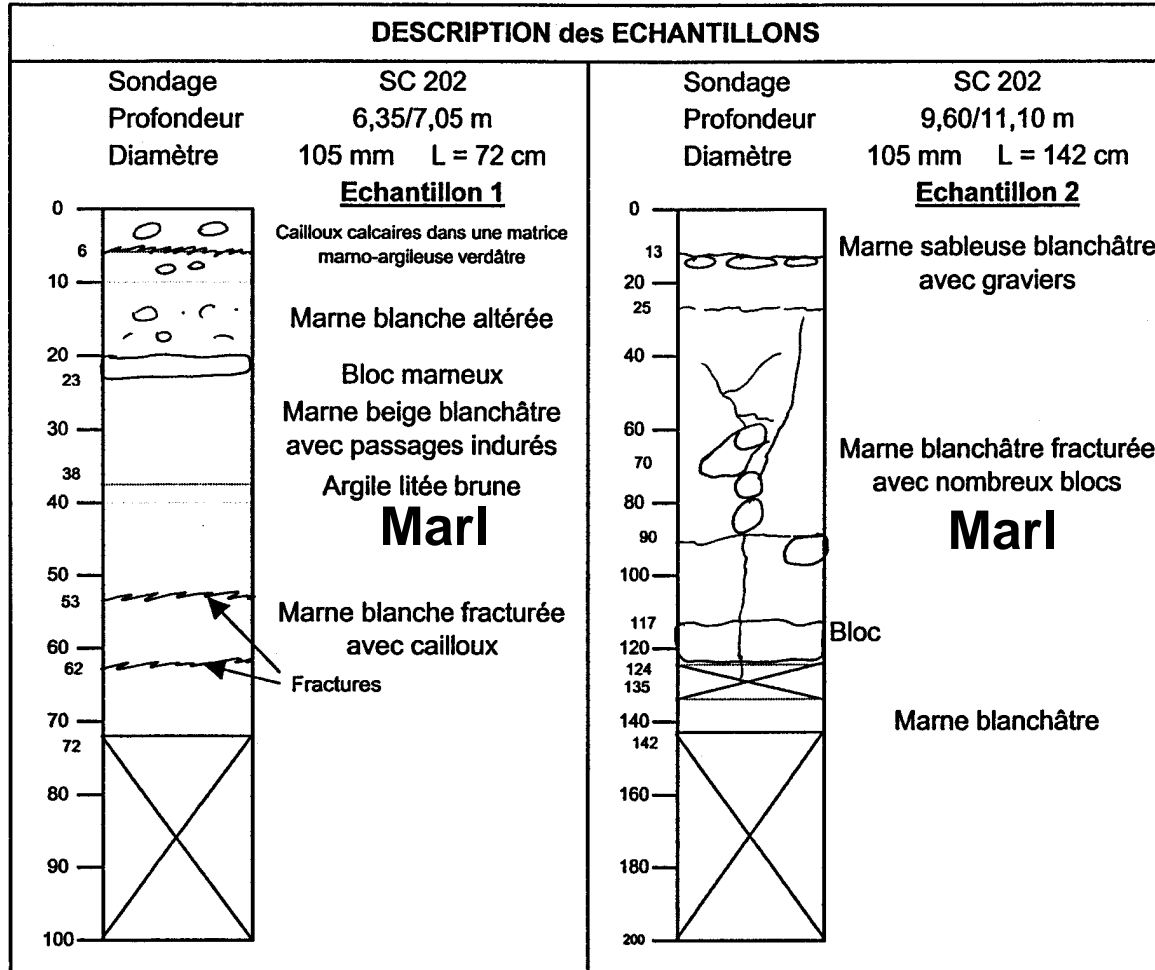


Bridge design



**Geotechnical data: 10^{-6} to 10^{-8}
of whole ground volume tested**

Geotechnical data



Identification of soils : core sampling results between abutment C0 and pier P1

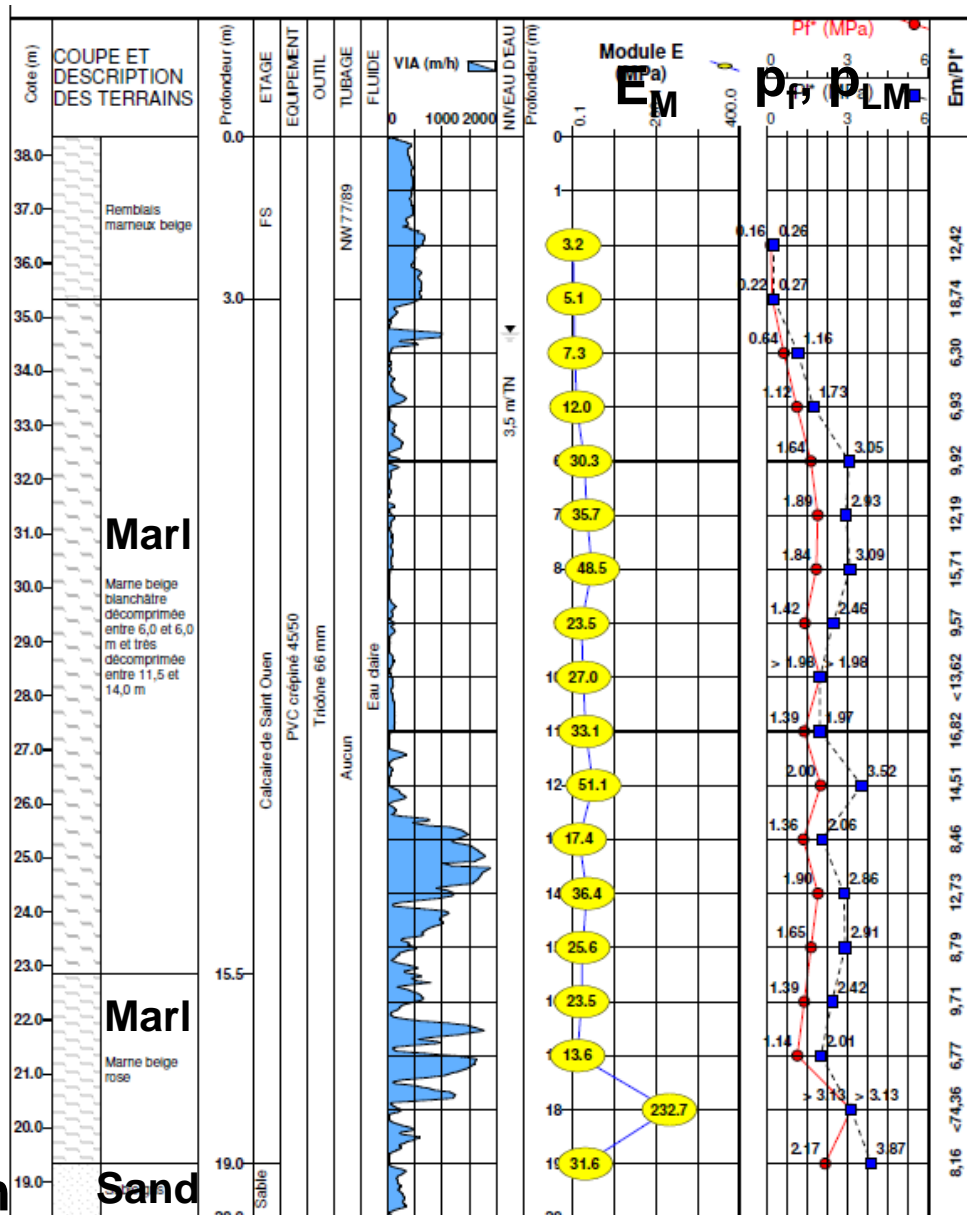
Geotechnical data



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z=0m

z=20m



Results of pressuremeter tests between abutment C0 and pier P1



Normally fractured **calcareous marl** (at 2,5 m depth and 3 m depth):

- $c'_{kg} = 0$ kPa
- $\varphi'_{kg} = 30$ degrees
- $\gamma_{kg} = 20$ kN/m³

From ground level to base of foundation: $\gamma = 20$ kN/m³

Water level is assumed to be one metre below the foundation level in both cases

Fill material : $c'_{kf} = 0$; $\varphi'_{kf} = 30$ degrees; $\gamma_{kf} = 20$ kN/m³

Some concluding comments



Eurocode 7 :

- a common language for the geotechnical engineers throughout Europe and on other continents...
- a tool for the dialogue between the structural engineers and the geotechnical engineers;
- yet geotechnical rules are mainly based on experience. Will the prevailing economic rules and the evolution of societies give the opportunity to further increase this experience ?



and to really conclude, Eurocode 7 states that:

2.4.1(2) “It should be considered that knowledge of the ground conditions depends on the **extent and quality of the geotechnical investigations**. Such knowledge and the **control of workmanship** are usually more significant to fulfilling the fundamental requirements than is precision in the calculation models and partial factors”.

&

1.3 “The code assumes that the personnel involved in all activities is suitably qualified and adequate communication exist among them”



Thank you for your attention !