ELABORATION OF MAPS FOR CLIMATIC AND SEISMIC ACTIONS FOR STRUCTURAL DESIGN IN THE BALKAN REGION



27-28 October 2015, Zagreb

General Principles of the Elaboration of Maps for Climatic and Seismic Actions

Paolo Formichi Convenor CEN/TC250/WG7 Basis of Structural Design



UNIVERSITÀ DI PISA



Overview of the presentation

- Climatic and Seismic Actions in the Eurocodes
- Reference Basis of Design
- General principles for the assessment of climatic actions. Examples for the snow load maps.
- Climate change influences.
- General principles for the assessment of seismic actions. Open points.





Links between the Eurocodes



Eurocode standards recognise the **responsibility of regulatory authorities in each Member State** and have safeguarded **their right to determine values related to regulatory safety matters at national level** where these continue to vary from State to State.

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National Annex - NDPs

ECs Foreword

The National annex may <u>only</u> contain information on those parameters which are left open in the Eurocode for national choice, known as Nationally Determined Parameters, to be used for the design of buildings and civil engineering works to be constructed in the country concerned, i.e. :

- values and/or classes where alternatives are given in the Eurocode,
- values to be used where a symbol only is given in the Eurocode,
- **country specific data** (geographical, climatic, etc.), e.g. snow map,

– the procedure to be used where alternative procedures are given in the Eurocode.

It may also contain:

- decisions on the application of informative annexes,
- references to non-contradictory complementary information to assist the user to apply the Eurocode.

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Distribution of NDPs in the ECs



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Basic requirements EN 1990

2.1(1)P A structure shall be designed and executed in such a way that it will, **during its intended life**, with appropriate degrees of reliability and in an economical way:

- sustain all actions and influences likely to occur during execution and use, and

– meet the specified serviceability requirements for a structure or a structural element.

2.1(2)P A structure shall be designed to have adequate :

- structural resistance,
- serviceability, and
- durability.

2.1(3)P Safety in case of fire

2.1(4)P Robustness

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"ULS" + "SLS"





1.5.2.2 design situations

sets of physical conditions representing the real conditions occurring during a certain time interval for which the design will demonstrate that relevant limit states are not exceeded

3.1(3)P Limit states shall be related to design situations

3.1(4) Design situations should be classified as **persistent**, **transient** or **accidental (seismic)**



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27-28 October 2015, Zagreb

Design Situations

1.5.2.3 Transient design situation

design situation that is relevant during a period much shorter than the design working life of the structure and which has a high probability of occurrence.

NOTE A transient design situation refers to temporary conditions of the structure, of use, or exposure, e.g. during construction or repair.











1.5.2.4 persistent design situation

design situation that is relevant during a period of the same order as the design working life of the structure.

NOTE Generally it refers to conditions of normal use.





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1.5.2.5 accidental design situation

design situation involving exceptional conditions of the structure or its **exposure**, including fire, explosion, impact or local failure



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1.5.2.7 seismic design situation

design situation involving exceptional conditions of the structure when subjected to a seismic event



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Actions, ULS Design situations



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ULS Persistent Transient Design Situations

$$\sum_{j\geq 1} \gamma_{G,j} G_{k,j} "+" \gamma_{P} P" +" \gamma_{Q_{1}} Q_{k,1} "+" \sum_{i\geq 1} \gamma_{Q,i} \psi_{0,i} Q_{k,i}$$
 Eq. (6.10)

or, alternatively for STR and GEO limit states, the less favourable of the two following expressions:

$$\begin{cases} \sum_{j\geq 1} \gamma_{G,j} G_{k,j} "+" \gamma_P P" +" \gamma_{Q,1} \psi_{0,1} Q_{k,1} "+" \sum_{i>1} \gamma_{Q,i} \psi_{0,i} Q_{k,i}) & \text{Eq.} \\ \\ \sum_{j\geq 1} \xi_j \gamma_{G,j} G_{k,j} "+" \gamma_P P" +" \gamma_{Q,1} Q_{k,1} "+" \sum_{i>1} \gamma_{Q,i} \psi_{0,i} Q_{k,i}) & \text{Eq.} \end{cases}$$

Eq. (6.10a)

Eq. (6.10b)





ULS Accidental Design Situations

$$\sum_{j\geq 1} G_{k,j} + P'' + Q'' + Q_{d''} + (\psi_{1,1} \text{ or } \psi_{2,1}) Q_{k,1} + \sum_{i>1} \psi_{2,i} Q_{k,i}$$

ULS Seismic Design Situations

$$\sum_{j\geq 1} G_{k,j} "+" P" + " A_{Ed}" + " \sum_{i\geq 1} \psi_{2,i} Q_{k,i}$$

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SLS Design Situations

Characteristic Combination



Frequent Combination

$$\sum_{j\geq 1} G_{k,j} "+"P"+"\psi_{1,l}Q_{k,1}"+"\sum_{i>1} \psi_{2,i}Q_{k,i}$$

Quasi Permanent Combination

$$\sum_{j\geq 1} G_{k,j} "+"P"+"\sum_{i\geq 1} \psi_2(Q_{k,i})$$

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Reliability Differentiation (Persistent)

EN 1990 Annex B

Table B2 - Recommended minimum values for reliability index β (ultimate limit states)

Reliability Class	Minimum values for β			
	1 year reference period	50 years reference period		
RC3	5,2	4,3		
RC2	4,7	3,8		
RC1	4,2	3,3		

NOTE A design using EN 1990 with the partial factors given in annex A1 and EN 1991 to EN 1999 is considered generally to lead to a **structure with a \beta value greater than 3,8 for a 50 year reference period**.

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Snow



Characteristic values of climatic actions

EN 19900 Note 2 to 4.1.2(7)P

The characteristic value of climatic actions is based upon the **probability of 0,02 of its time-varying part being exceeded for a reference period of one year**. This is **equivalent to a mean return period of 50 years** for the time-varying part. However in some cases the character of the action and/or the selected design situation makes another fractile and/or return period more appropriate.

$Q_k = Q_{50yrs}$ Design Working Life \neq Return Period

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Other Representative Values of variable (climatic) actions



 $\begin{array}{l} \psi_0 \ Q_k \ Combination \ value \\ \psi_1 \ Q_k \ Frequent \ value \\ \psi_2 \ Q_k \ Quasi \ Permanent \ value \end{array}$

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Many clauses of EN 1991-1-3 are based on the results of a research work, carried out between 1996 and 1999, under a contract specific to this Eurocode, to DGIII/D3 of the European Commission.

They were identified four main research items:

- □ study of the **European ground snow loads map**
- □ investigation and treatment of **exceptional snow loads**
- □ study of conversion factors from ground to roof loads
- □ definition of ULS and SLS combination factors for snow loads.





Needs for harmonization – Development of European ground snow load map

- Inconsistencies at borders between existing national maps;
- Different procedures for measuring snow load (mainly ground snow data): snow depths + density conversion, water equivalent measures, direct load measures;
- Different approaches for statistical data analysis (Gumbel, Weibull, Log-normal distributions).

The research developed a consistent approach Produced regional maps (Annex C of EN 1991-1-3)

Snow load with Altitude relationship

Zone numbers & altitude functions

Geographical boundaries

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For maps in Annex C of EN 1991-1-3 the following common approach has been followed:

- Statistical analysis of yearly maxima, using the Gumbel Type I
 CDF (best fitting in the majority of data points);
- □ **LSM** for the calculation of the best fitting regression curve;
- Both zero and non zero values have been analysed according to the "mixed distribution approach";







ELABORATION OF MAPS FOR CLIMATIC AND SEISMIC ACTIONS FOR STRUCTURAL DESIGN IN THE BALKAN REGION Regionalization of CEN area (18 countries 1997) into 10 climatic regions;
 Smoothing of maps across borderlines between neighbouring climatic regions (buffer zones 100 km).





2'600 weather stations







In some regions, particularly southern Europe, isolated very heavy snow falls have been observed resulting in snow loads which are significantly larger than those that normally occur. Including these snowfalls with the more regular snow events for the lengths of records available may significantly disturb the statistical processing of more regular snowfalls.



Gumbel probability paper: *Pistoia* (*IT*)

 N° of recorded years = 51

 N° of no snowy winters = 26

 $s_m = Max. snow Load = 1.30 kN/m^2$

50yrs load incl. Max Load = 1.00 kN/m²

 $s_k = 50$ yrs load excluded Max Load = 0.79 kN/m²

$$k = s_m / s_k = 1,65$$





Location of weather stations (159) where exceptional ground snow loads were detected (1996-1999)

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20%

18%

16%

14%

12%

10%

8%

6%

4%

2%

0%

Frequen za

Which PDF?



Latitude

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Alpine Region – Snow load at sea level



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Map for Mediterranean region Annex C EN 1991-1-3

(geographical boundaries)

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Italian National Annex (administrative boundaries)





Italian ground Snow load Map:

- -4 different zones (3 Med. + 1 Alpine)
- -Administrative boundaries (110 provinces)

-4 Altitude correlation functions







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- The digital map is applicable also for **direct probability assessments of structures**:
 - a) characteristic value of the snow load on the ground (s_k) (based on 1961-2009 obs.)
 - b) statistical characteristics for the distribution of annual maximum of snow load on the ground:
 - mean value μ,
 - standard deviation σ,
 - coefficient of variation V,
 - skewness a

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Rigiona ()	At	16	81	82	Q.5	-58	Ð	10
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Figure C.7





Consistency at borders?

Figure C.3

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Maps given in National Annexes are determined without taking into account "**exceptional falls**"

How to determine design values for accidental ground snow loads?

For locations where exceptional loads may occur (**National Annex**), the ground snow load may be treated as accidental action with the value:

$$s_{Ad} = C_{esl} s_k$$

Where:

 C_{esl} (set by the National Annex) - recommended value = 2,0 s_k = characteristic ground snow load at the site considered

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Slovakia

Locations of weather stations with recorded exceptional snow loads (85 over 660)

Region	1	2	3	4
Coefficient C_{esl}	2.1	2.2	2.5	3.7







1900

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2000



Climate change - Vulnerability of buildings in Norway (SINTEF 2013)



% variation of 50-yrs ground snow load in the periods: 1961-1990 / 1981-2010 + predictions according IPCC scenarios

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Climate change - Vulnerability of buildings in Norway (SINTEF 2013)

Estimate of ground snow load variation (resulting from 3 IPCC scenarios) in the **period 2071-2100** compared to the current Norwegian Annex to EN 1991-1-3



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Interaction of Extreme Weather Events (**EWE**)

M515 Next Generation of ECs: Climate Change Objectives

Climate change	This will provide increased resilience of long-life infrastructure assets
consideration embraced	to potential climatic changes. It is very cost effective to address such
within Eurocodes	risks at the design stage rather than through later retrofitting. Such
	an approach also reduces user disruption and environmental impacts.

- Report on the impact of climate change on climatic actions in relation to structural design issues.
- Modified or additional clauses for EN 1991-1-3, -1-4, -1-5 and EN 1991-1-9 (Atmospheric Icing) (and possibly other Eurocode Parts).
- Background document(s)

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EN 1990 4.1.2(9) For seismic actions the design value A_{Ed} should be assessed from the characteristic value A_{Ek} or specified for individual projects.

NOTE See also EN 1998.

 $\mathbf{A}_{Ed} = \gamma_T \mathbf{A}_{Ek}$

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EN 1998-1

2.1(1)P Structures in seismic regions shall be designed and constructed in such a way that the following requirements are met, each with an adequate degree of reliability.

- No-collapse requirement.

The design seismic action is expressed in terms of: a) the reference seismic action associated with a reference probability of exceedance, P_{NCR} , in **50 years or a reference return period**, T_{NCR} , and b) the **importance factor** γ_{I} (.....) to take into account reliability differentiation.

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– No-damage requirement...

P _{DLR}, in 10 years or a reference return period, T _{DLR}

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EN 1998-1

NOTE 1 The values to be ascribed to P_{NCR} or to T_{NCR} for use in a country may be found in its **National Annex** of this document. The recommended values are $P_{NCR} = 10\%$ (50 yrs ref. period) and $T_{NCR} = 475$ years.

NOTE 3 The values to be ascribed to P_{DLR} or to T_{DLR} for use in a country may be found in its **National Annex** of this document. The recommended values are $P_{DLR} = 10\%$ (10 yrs ref. period) and $T_{DLR} = 95$ years.

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EN 1998-1

2.1(2)P **Target reliabilities** for the no-collapse requirement and for the **damage limitation requirement** are **established by the National Authorities** for different types of buildings or civil engineering works on the basis of the **consequence of failure**.

2.1(3)P **Reliability differentiation** is implemented by classifying structures into different **importance classes**. An importance factor γ_{I} is assigned to each importance class.

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Reliability Differentiation

EN 1998-1

The value of the importance factor $\gamma_{\rm I}$ multiplying the reference seismic action (PGA) to achieve the same probability of exceedance in $T_{\rm L}$ years as in the $T_{\rm LR}$ years for which the reference seismic action is defined, may be computed as $\gamma_{\rm I} \sim (T_{\rm LR} / T_{\rm L})^{-1/k}$.

3.2.1 Seismic zones

EN 1998-1

(1)P For the purpose of EN 1998, national territories shall be subdivided by the National Authorities into **seismic zones**, **depending on the local hazard**. **By definition**, the hazard within each zone is assumed to be constant.

(2) For most of the applications of EN 1998, the hazard is described in terms of a single parameter, i.e. the value of the reference peak ground acceleration on type A ground, a_{gR} . Additional parameters required for specific types of structures are given in the relevant Parts of EN 1998.

NOTE The reference peak ground acceleration on type A ground, a $_{gR}$, for use in a country or parts of the country, may be derived from zonation maps found in its **National Annex**.

- 1. Specification of the models for the seismic sources responsible for the seismic hazard
- 2. Specification of the ground motion models (attenuation relationships)
- **3.** Calculation of the reference parameter (PGA) for the given probability of exceedance

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1. Specification of the models for the seismic sources responsible for the seismic hazard

Seismogenic sources

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- Source : ITAS308 Events in AS: 123. Complete : 52 Cum, FMD 0 Non-Cum EMD _ b_{pml} = 0.98, a_{pml} = 3.92 b = 1.a = 4.210 Weighted Mean FMD events 1/[year] 10 Latitude Number of 10 10 10 14 15 16 11 12 13 Magnitude Longitude
- Statistical description of the seismic hazard for a given location based on earthquake catalogues
- Gutenberg-Richter relationship
- pdf f(m) of events up to a given magnitude (m)

2. Specification of the ground motion models (attenuation relationships)

The attenuation relationships provide the value of a ground motion parameter (peak ground acceleration, spectral ordinates...) at a certain Distance (R) from an earthquake of a given magnitude (M)

Empirically determined equations e.g. Ambraseys (1996) for intraplate seismicity in Europe

Statistical estimate of PGA, given the occurrence of a seismic event with a specific magnitude (M) and at a given distance (R) from the site being considered

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3. Calculation of the reference parameter (PGA) for the given probability of exceedance

Assumptions:

- Each seismic event can take place at any time
- Any seismic event is independent of the occurrence of all others
- Recurrence frequency of seismic events in a given time interval Td is given by λ Td, being $\lambda = 1/Tr$ the mean recurrence frequency of the seismic event assumed to be constant
- Events follow a Poisson process

By numerical integration it is possible to evaluate the seismic hazard, in terms of probability of exceedance of a PGA, for each site and for a given time interval.

Hazard curves

3. Calculation of the reference parameter (PGA) for the given probability of exceedance

The Italian example

Hazard curves are not homothetic, they change with the return period

Seismic zonation based only upon TR475 PGA values is not fully representative

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The Italian approach

Probability of exceedance 10% in 50 yrs

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From seismic zones to the definition of local seismic hazard

Italian territory divided in 10'571 grid points (grid span 5 km)

For each grid point derived hazard curves for different probability of exceedance

Open points:

- Inconsistencies at borders between neighbouring countries
- Different presentation of seismic maps
- Harmonization of procedures and/or parameter values is highly desirable

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Future evolution of EN 1998-1 (M515)

The main benefit of this action is to update the way in which the seismic zonation is presented, taking profit of the more recent research in this field and aligning EN1998 with the way in which seismic zonation is presented in other national and international seismic codes.

To this effect profit shall be taken from recent European research projects, namely the **project SHARE**, which provided **consistent methodologies and tools to support the establishment of a European seismic zonation**.

Redrafting of Section 3 (Ground conditions and Seismic action) of EN 1998-1.

The redrafting shall provide the advancement towards a harmonized seismic zonation but still enabling the Member States, if required, to establish its own safety levels at different performance levels and for different types of structures (importance classes).

European Commission

Thank you for your attention

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